

Test design and planning using NHERI WOW EF: Aeroelastic, Aerodynamic, Destructive and Wind-Driven Rain Tests

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(WOW-EF, FIU)**

**August 11, 2020
9:00 – 9:20pm PDT**



- Existing Testing Capabilities:

- Aerodynamic Test
- Aeroelastic Test
- Wind-Driven Rain Test
- Destructive Test

- Recent and Scheduled Upgrades:

- Automated Roughness
- Robotic Arm
- PIV (MRI)
- Downburst Simulator

Aerodynamic Test

- Example Project: Wind Effects on Canopies Attached to Low/Mid-Rise Buildings
 - Complex flow: canopy/building interaction
 - Top/bottom surface taps (differential wind pressure) → C&C loads
 - **Net** wind effect → Overall design



- Example Project: Wind Effects on Balconies (Multi-Scale)



1:180

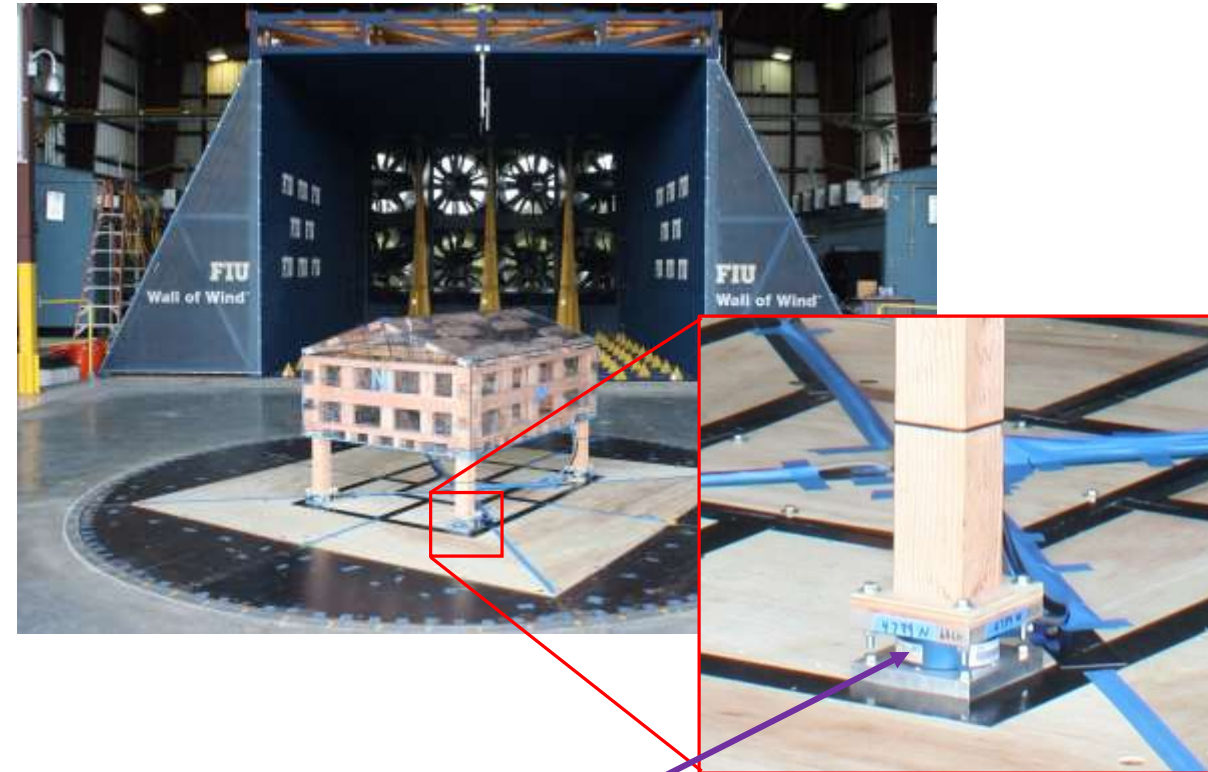


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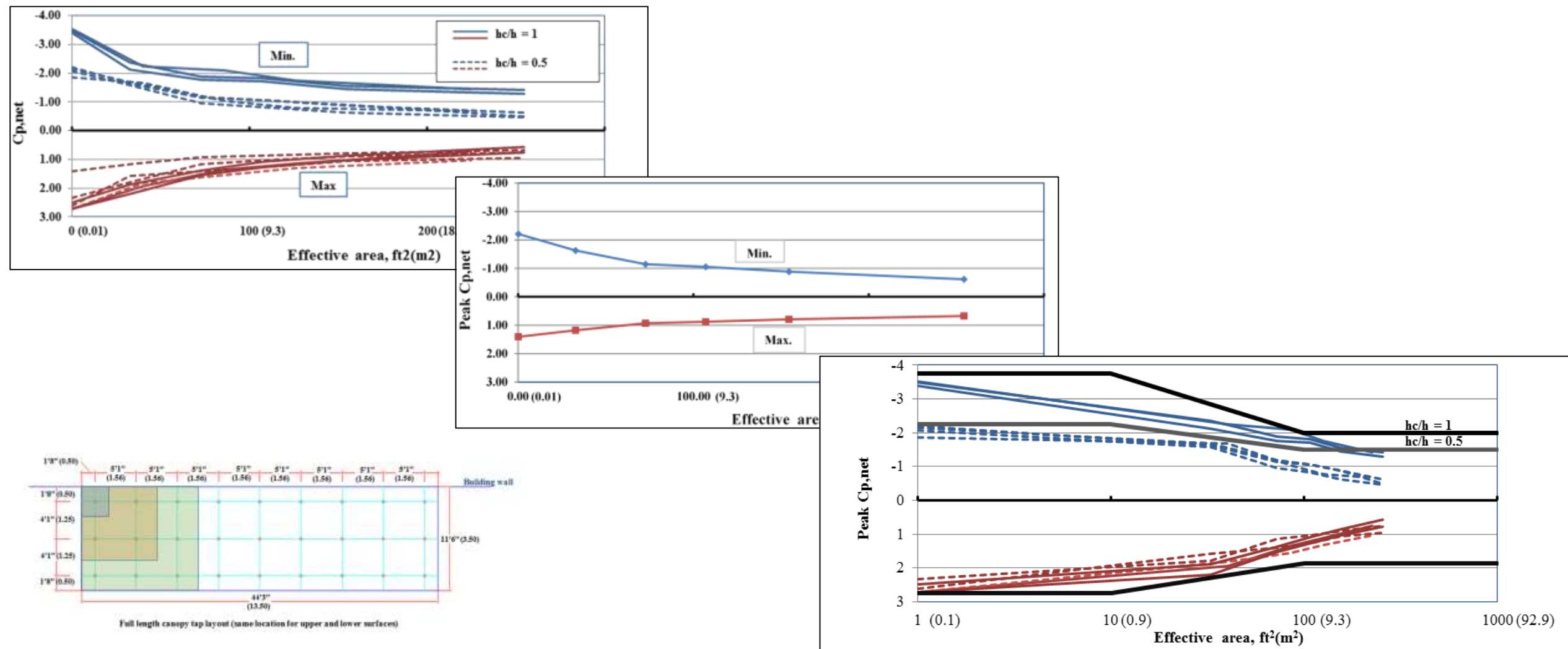
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- Example Project: Wind Effects on Elevated Houses



MDOF Load Cell

- Sample Results (used for Codification):



Aeroelastic Test

- Certain structures may experience significant aerodynamic forces generated by structural motions.
- These motions, called self-excited, are in turn affected by the aerodynamic forces they generate.
- The structural behavior associated with self-excited motions is called aeroelastic.
- Aero-elastic testing is the most reliable approach to predict the structural deformation and aeroelastic feedback under wind actions.



Aero-elastic Model Design

Motivations

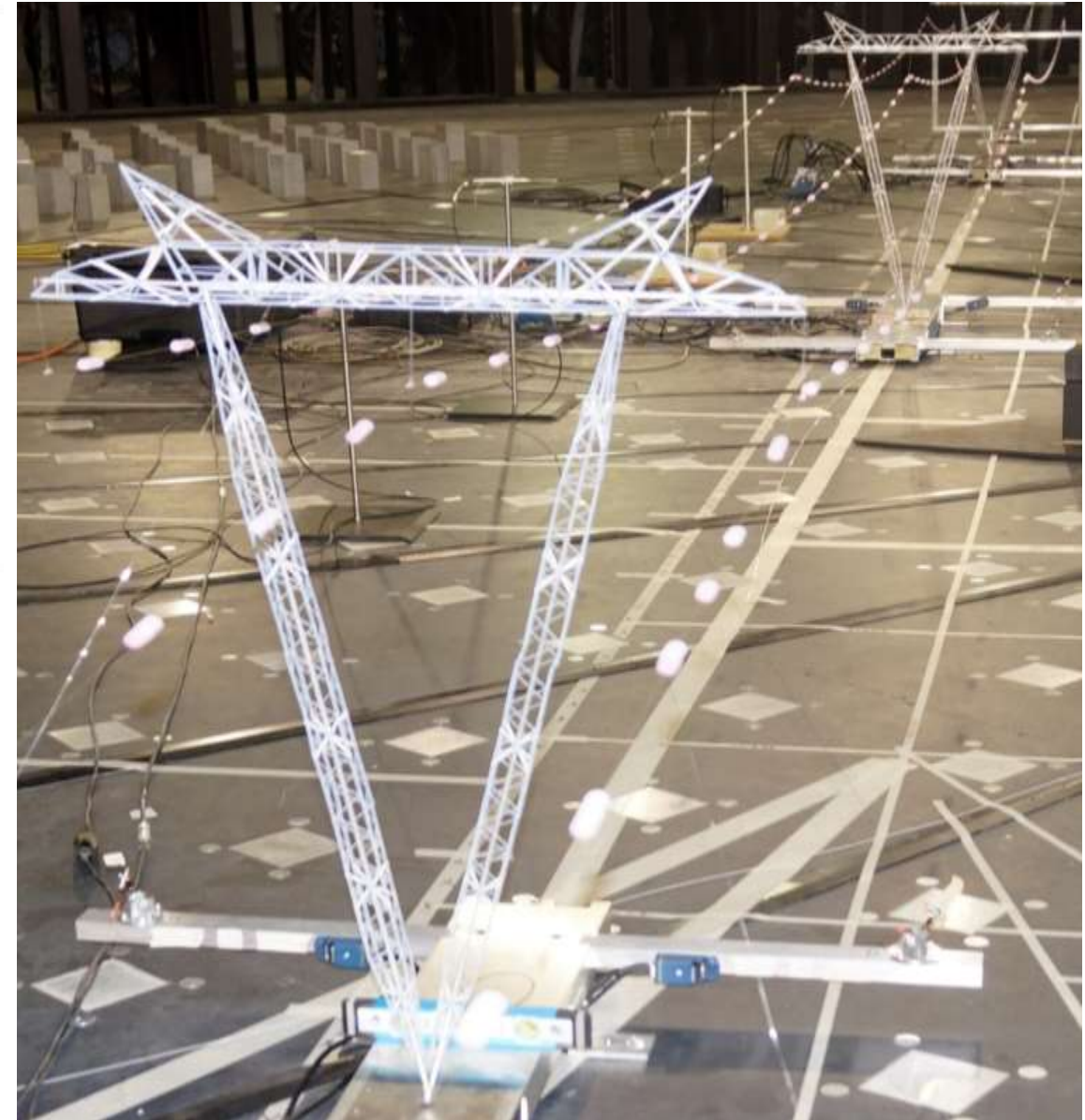
Length Scale
(shape of building)

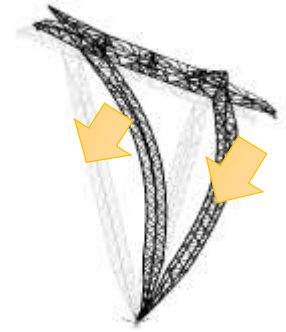
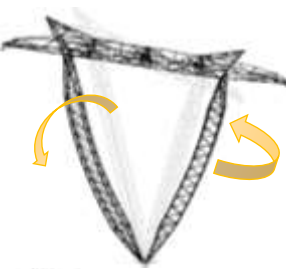
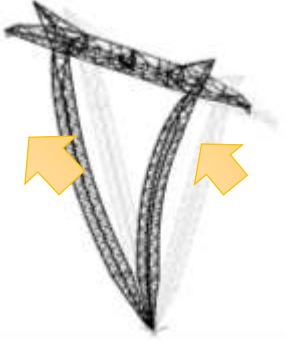
Mass, mass
moment of
inertia, damping

Velocity Scale

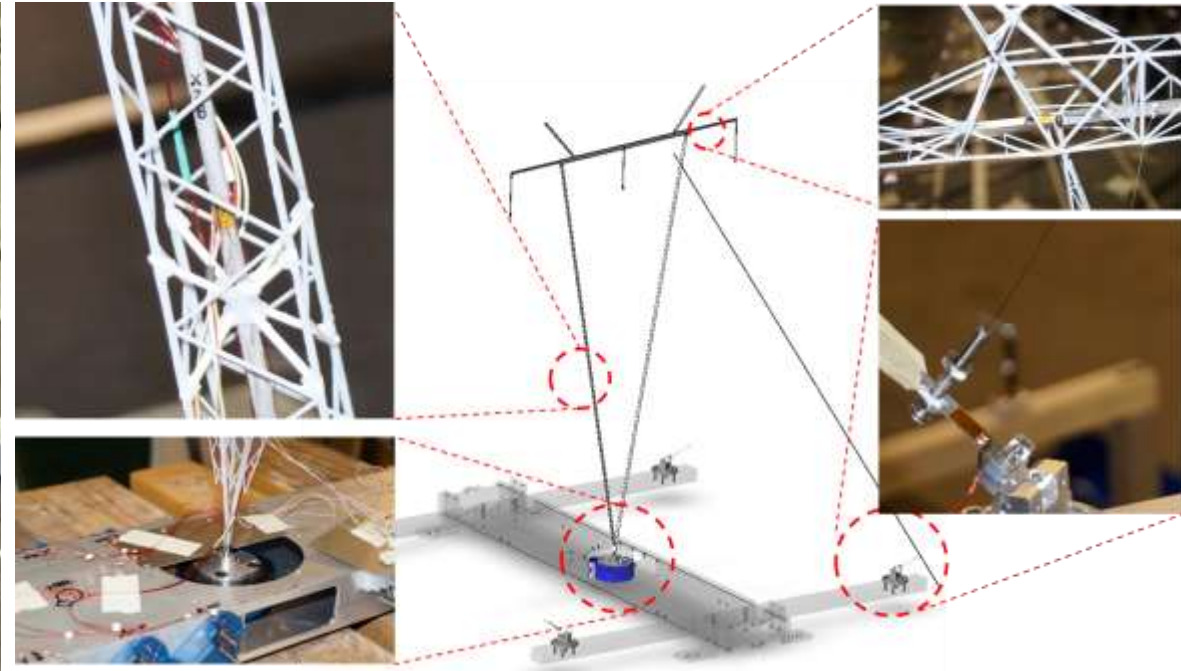
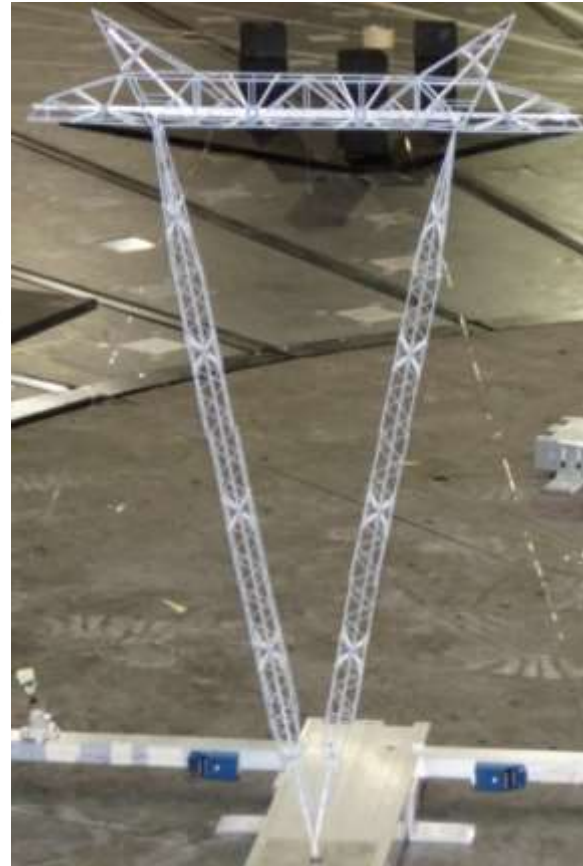
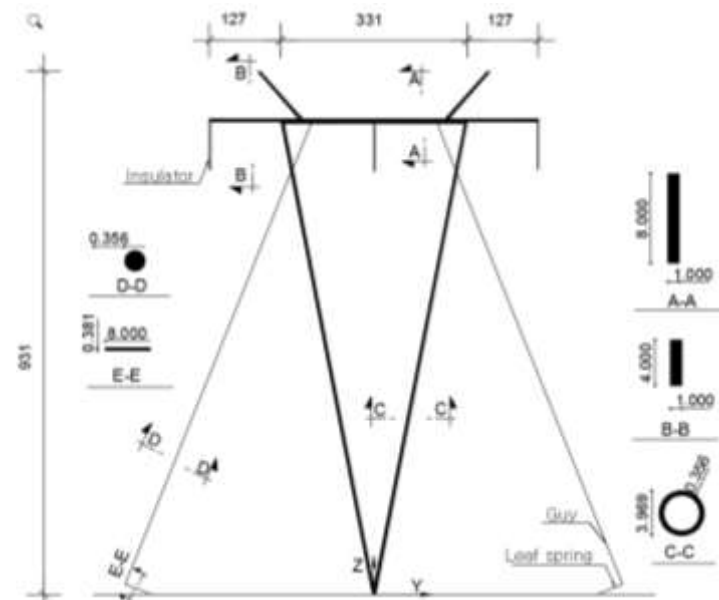
Moments, shear
forces, and
accelerations

Parameters	Similitude Requirements	Scaling Ratio
Length	$\lambda_L = L_m / L_f$	1: 50
Velocity	$\lambda_V = \lambda_L^{0.5}$	1: 7.07
Time	$\lambda_T = \lambda_L / \lambda_V$	1: 7.07
Density	$\lambda_\rho = \rho_m / \rho_f$	1: 1
Mass	$\lambda_M = \lambda_\rho \lambda_L^3$	1: 125,000
Mass Moment of Inertia	$\lambda_I = \lambda_M \lambda_L^2$	1: 312,500,000
Acceleration	$\lambda_a = \lambda_V / \lambda_T$	1: 1
Damping	$\lambda_\zeta = \zeta_m / \zeta_f$	1: 1
Axial Stiffness	$\lambda_{EA} = \lambda_V^2 \lambda_L^2$	1: 125,000
Bending Stiffness	$\lambda_{EI} = \lambda_V^2 \lambda_L^4$	1: 312,500,000
Force	$\lambda_F = \lambda_V^2 \lambda_L^2$	1: 125,000
Force / m'	$\lambda_f = \lambda_V^2 \lambda_L$	1: 2500
Bending and Torsional Moment	$\lambda_{BM-TM} = \lambda_V^2 \lambda_L^3$	1: 6,250,000
Warping Stiffness	$\lambda_{CW} = \lambda_V^2 \lambda_L^6$	1: 781,250,000,000

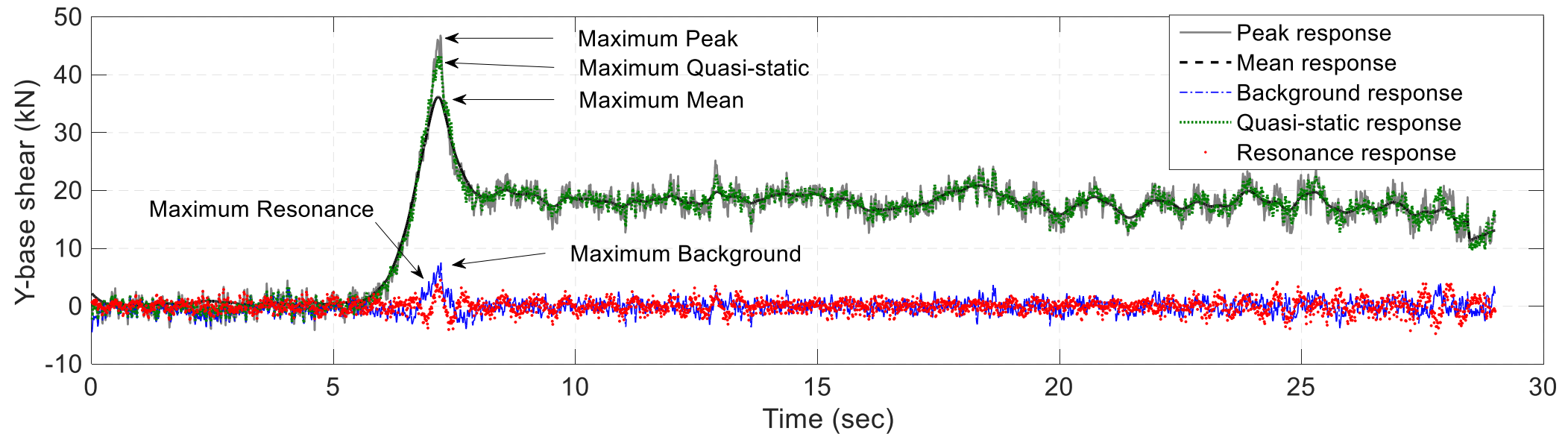
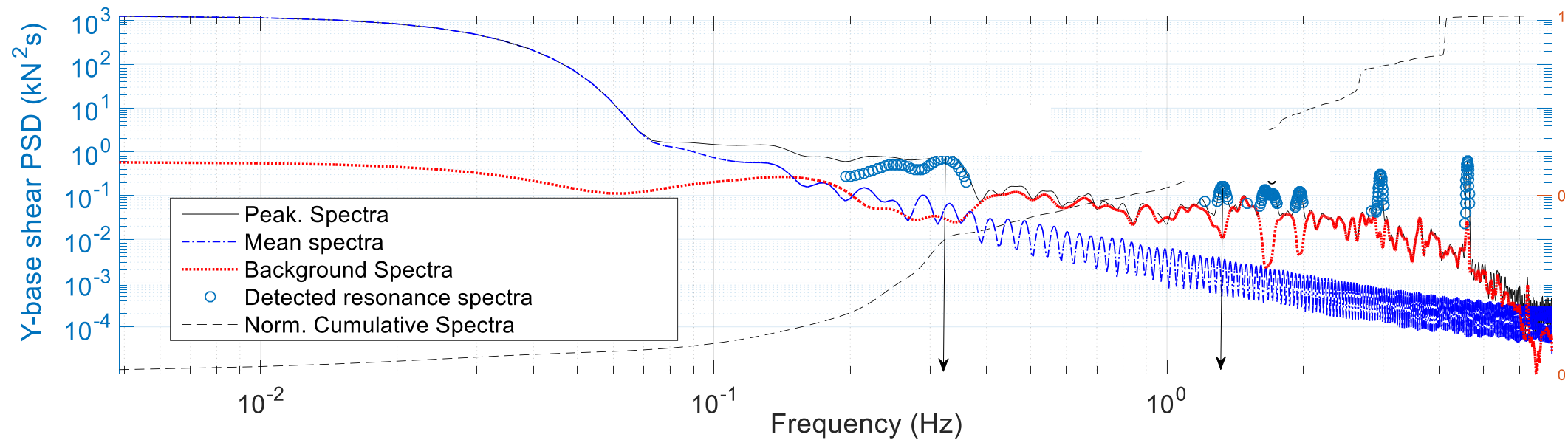


Mode	Shape	Prototype Frequency (Hz)	Frequency scale	Target Frequency (Hz)
1		1.44	1/Time Scale=7.07	$1.44 \times 7.07 = 10.18$
2		1.88		$1.88 \times 7.07 = 13.3$
3		2.44		$2.44 \times 7.07 = 17.25$

Equivalent Reduced Scale Model

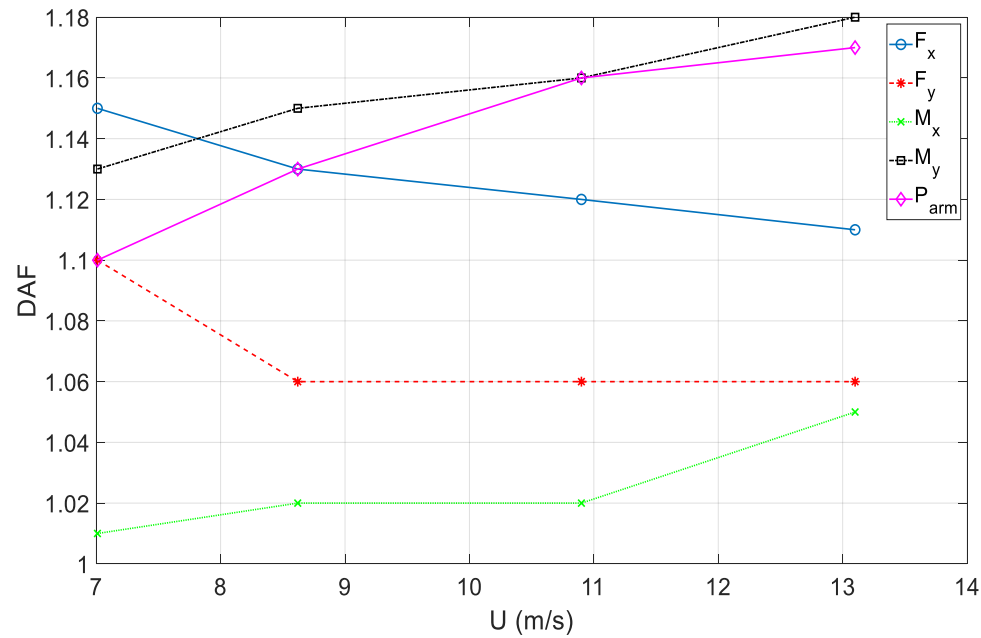


Expected Outcomes from an aero-elastic testing

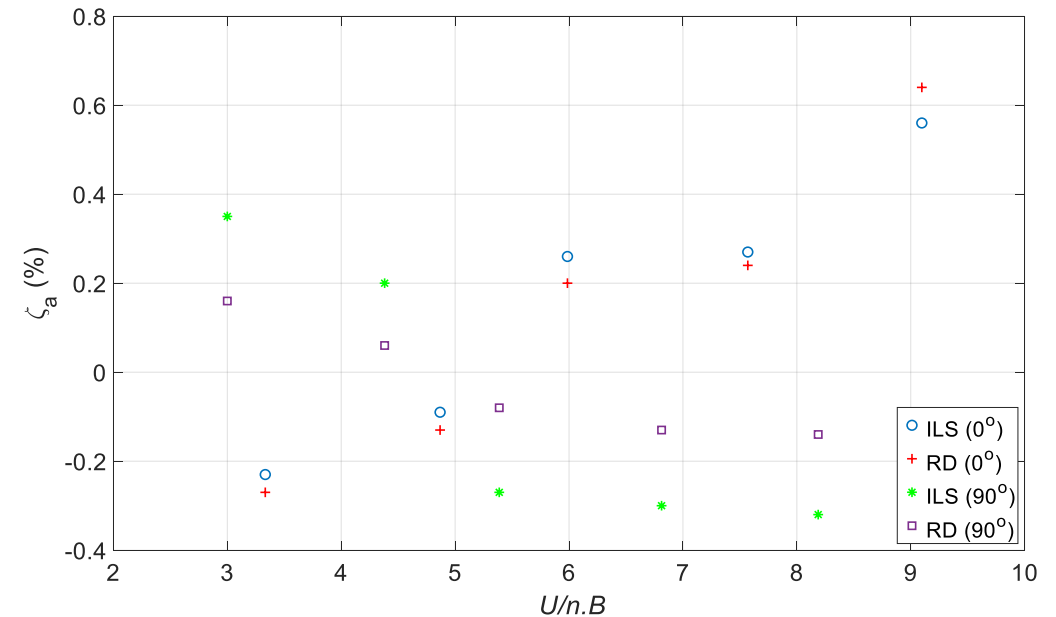


Expected Outcomes from an aero-elastic testing

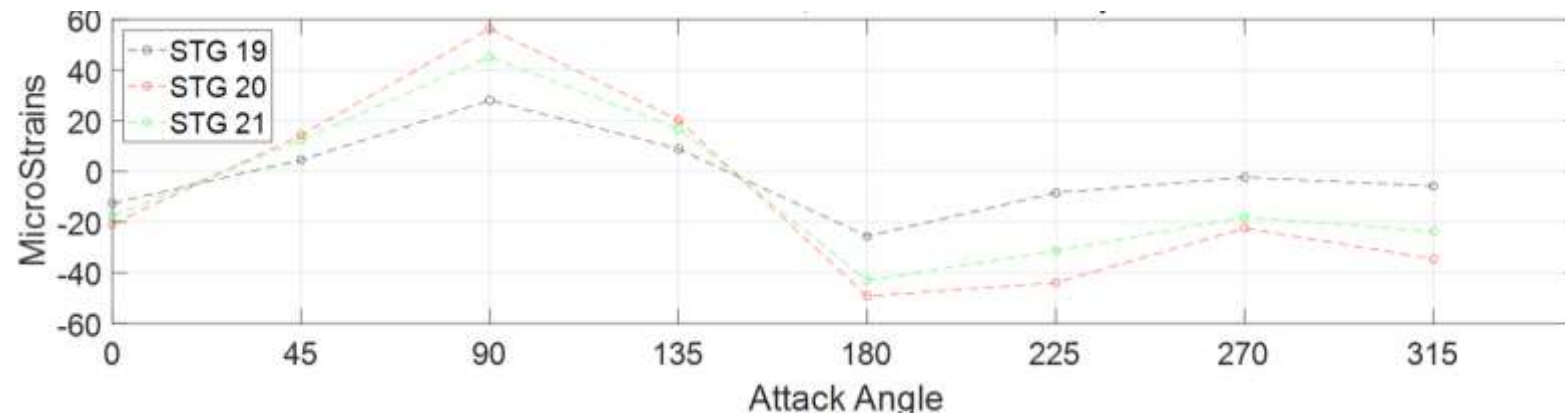
$$DAF = \frac{(\text{Maximum Peak Response})}{(\text{Maximum Quasi static Response})}$$



Damping and aerodynamic damping



Strain Measurements



Wind-Driven Rain Test

Steps:

- Determine target wind-driven rain parameters (characteristics of rain associated with tropical storms and hurricanes have been studied by many researchers)
- Selection of nozzles to simulate the target WDR parameters

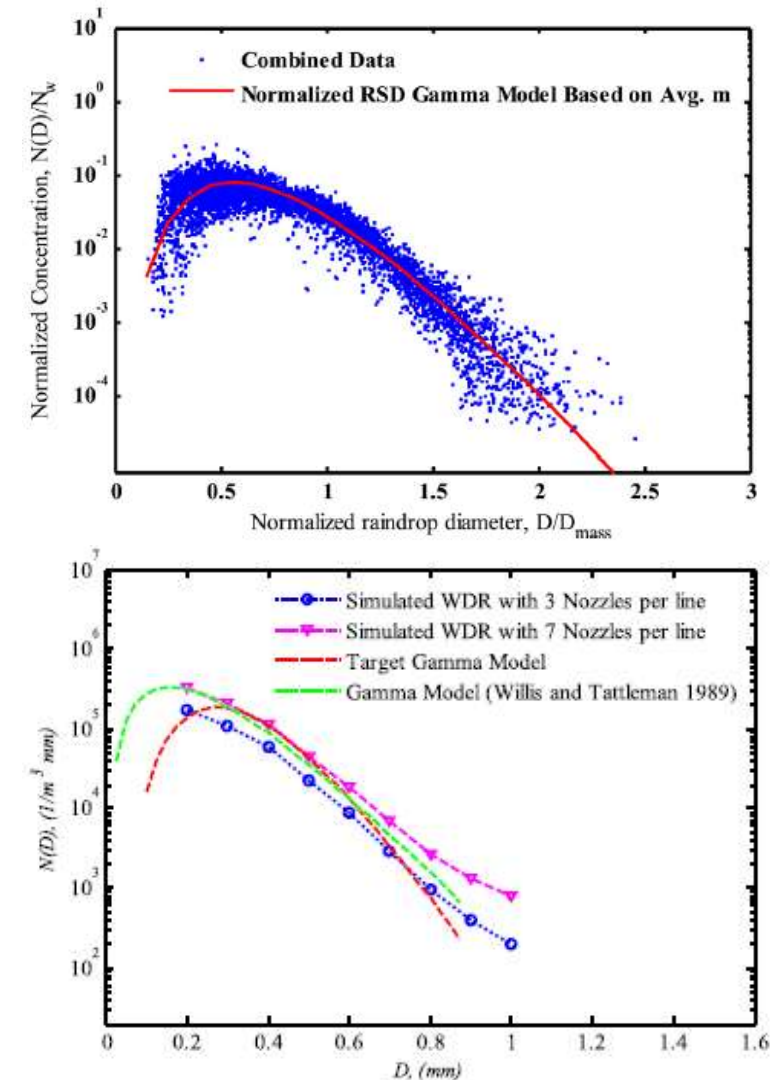


Fig. 10. RSD of simulated WDR using TEEJET 8008 – E nozzles.



Wind-Driven Rain Test of Full-Scale Model

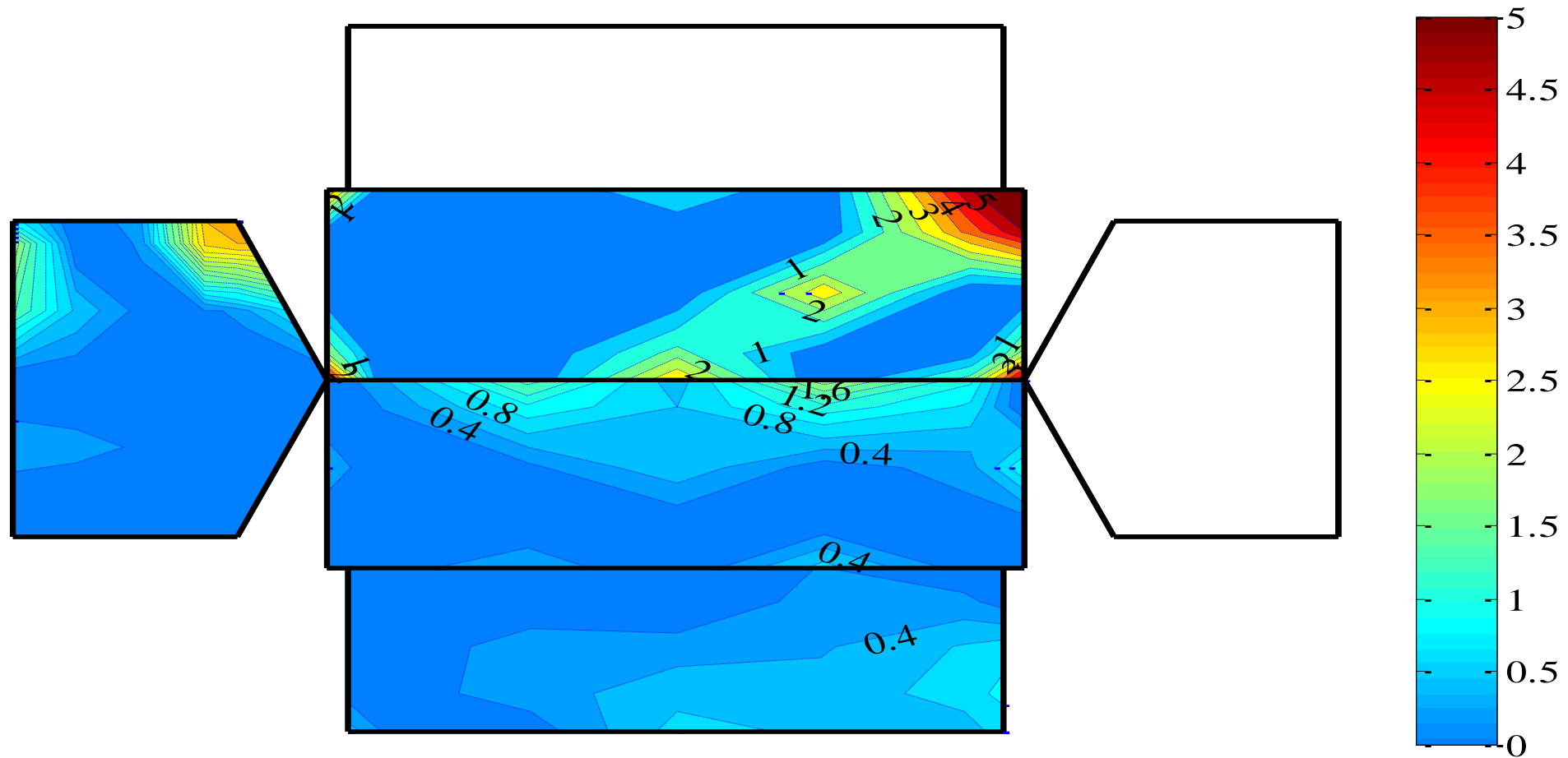


Large-Scale Model with Rain Gauges



Water-Injection System for Wind-Driven Rain

- Sample Results (Exterior)

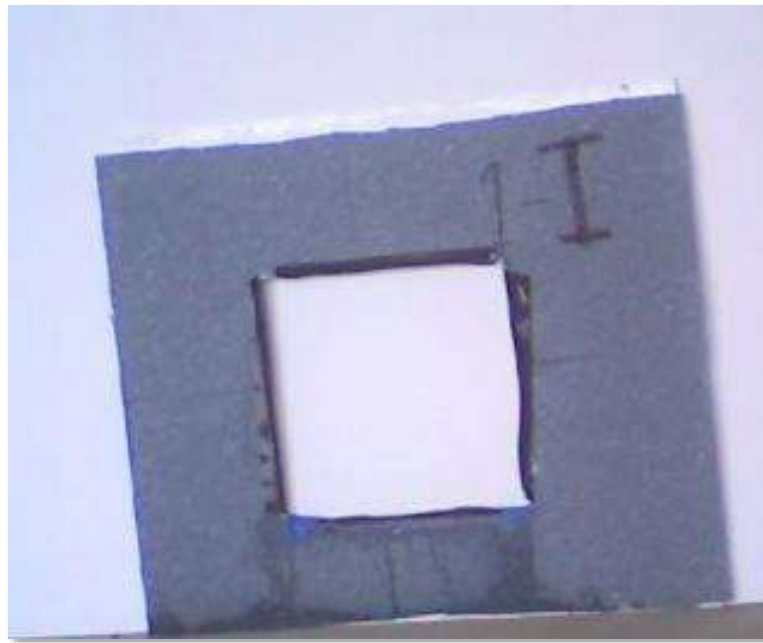


Findings: The leading edge/corner regions receive less volume surface runoff rainwater; The rain water accumulation increases toward the leeward roof surfaces.

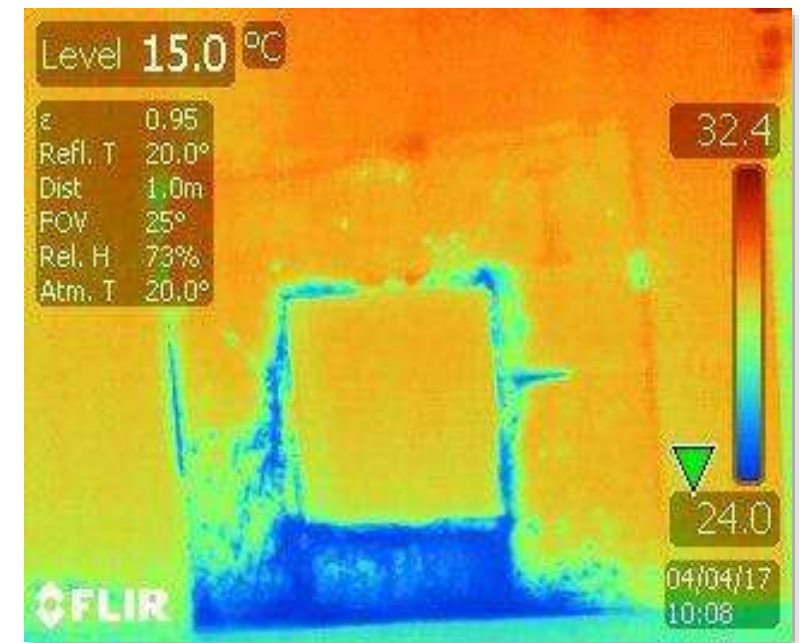
- Sample Results (Interior)



Internal walls covered with dried absorbent pads

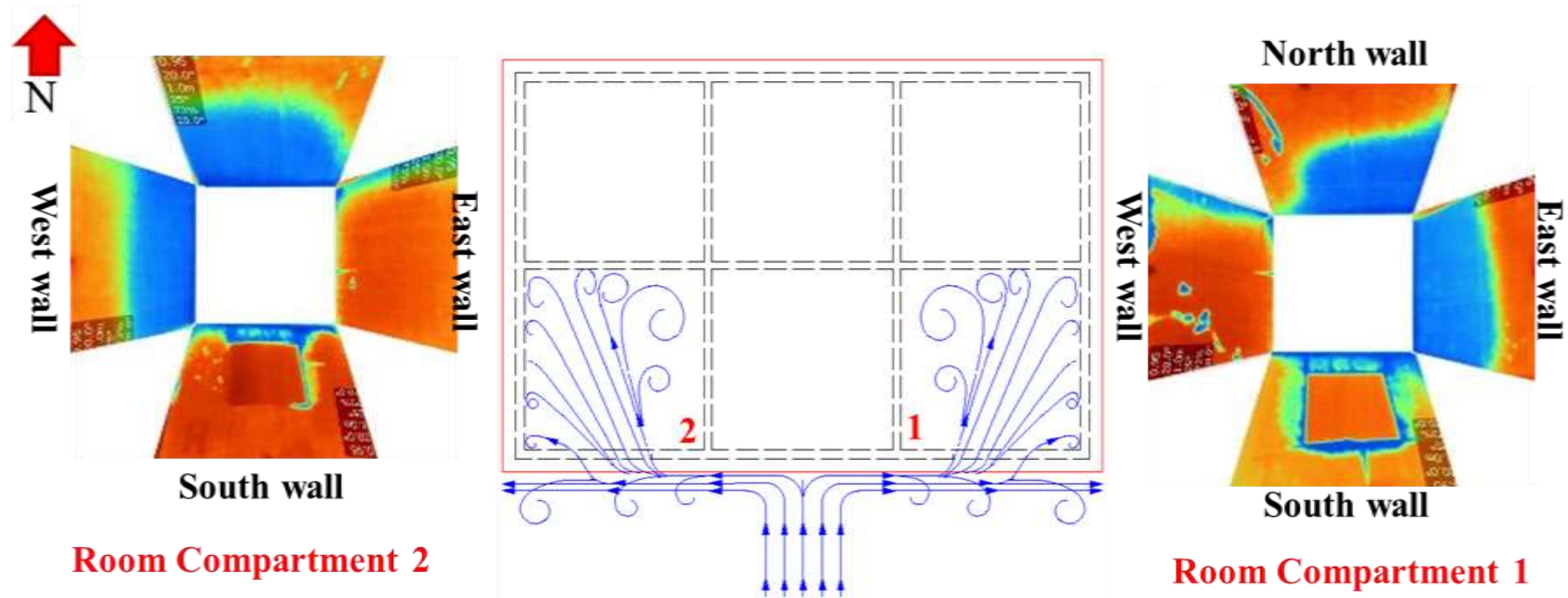


Remove and weight the wet pads after each test

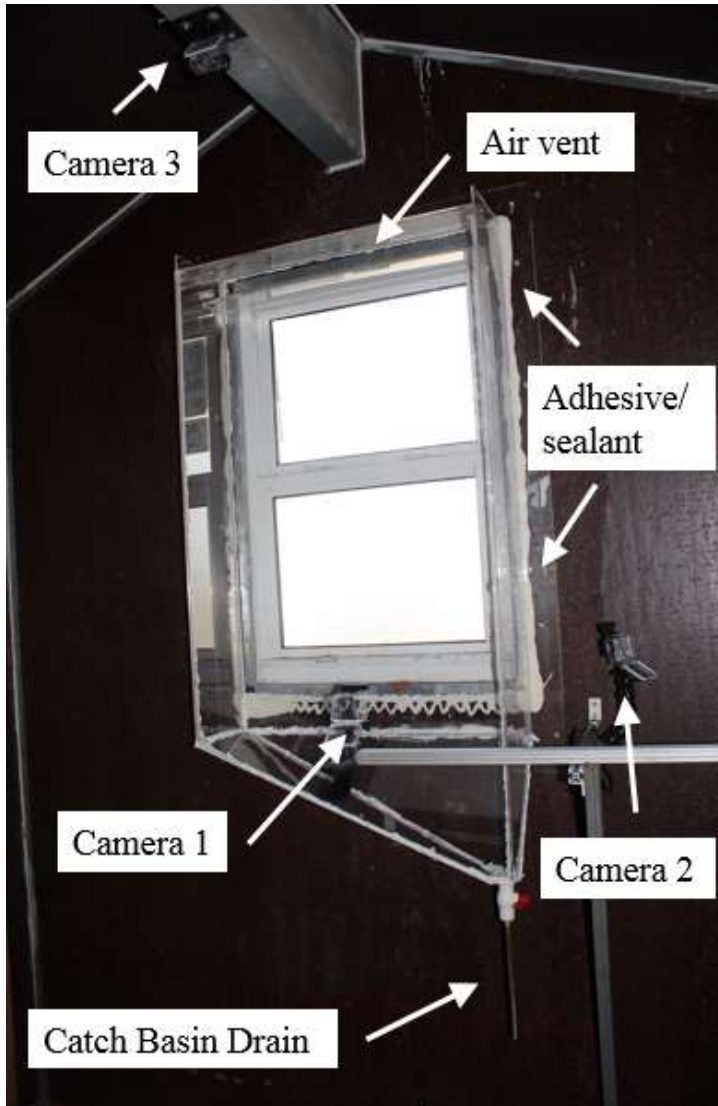


Take thermographic pictures

- Sample Results (Interior)



- Instrumentation and WDR Intrusion Results:

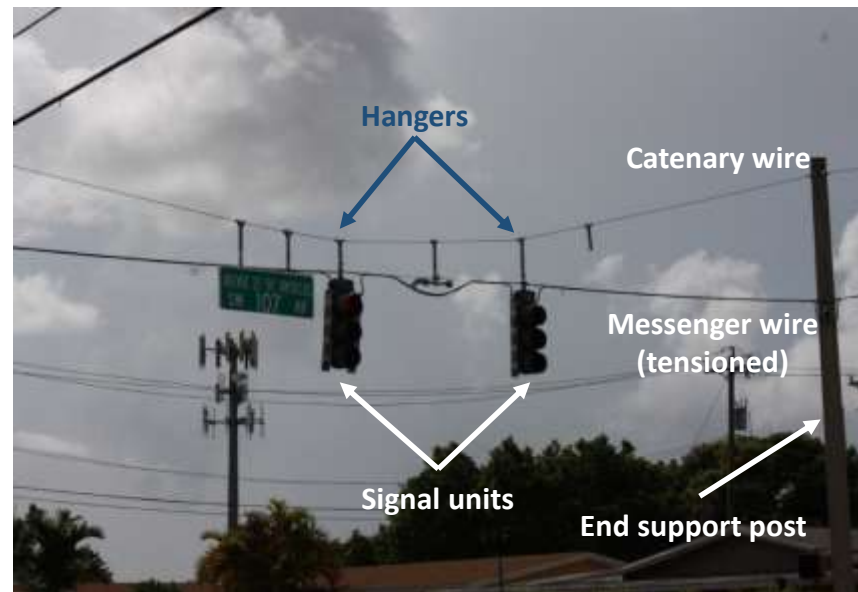


Comparison of water intrusion collected in catch basin for 0° wind direction, 62 mph test case.

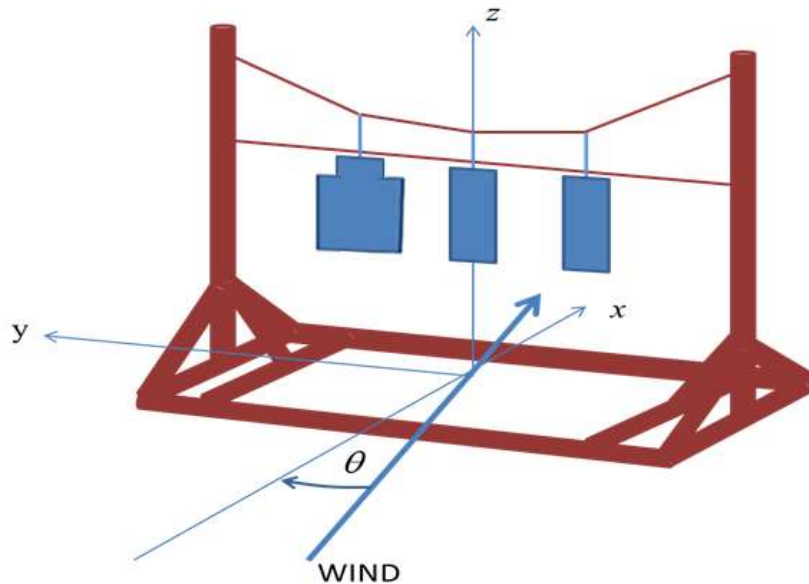
- a) Nonimpact window,
- b) Accordion shutter.

Destructive Test

- Traffic signals are an important part of civil infrastructure
- In 2003-2004, hurricanes with wind speeds exceeding 100 mph caused considerable damage to traffic signals in Florida and other states
- Failure of the signal systems results in unsafe traffic conditions during and after a storm, and the time taken for repairs delays recovery
- Span wire traffic signals are widely being used in the state of Florida and other states in USA



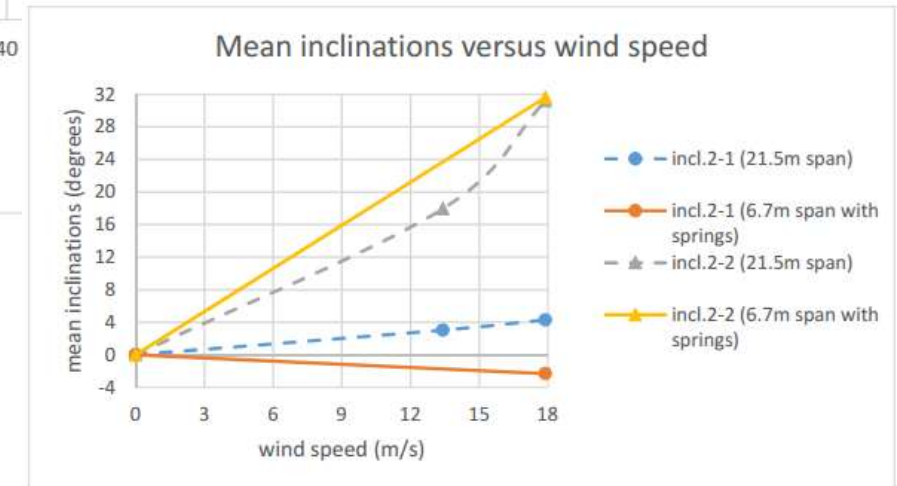
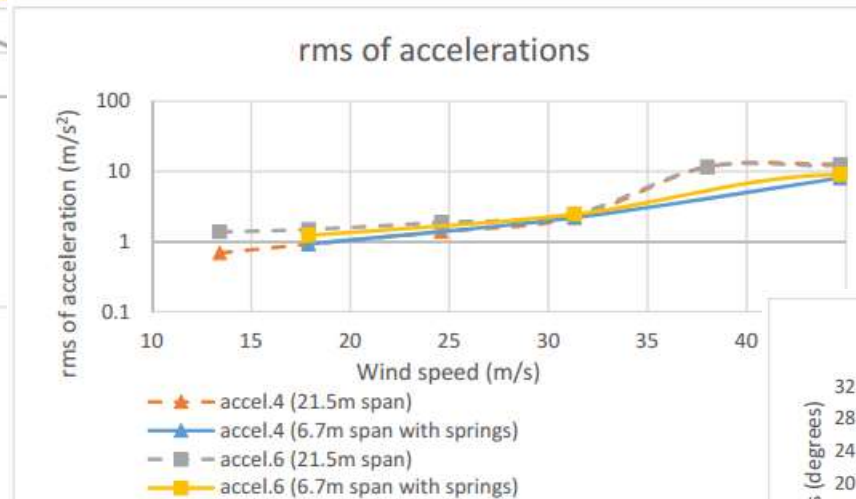
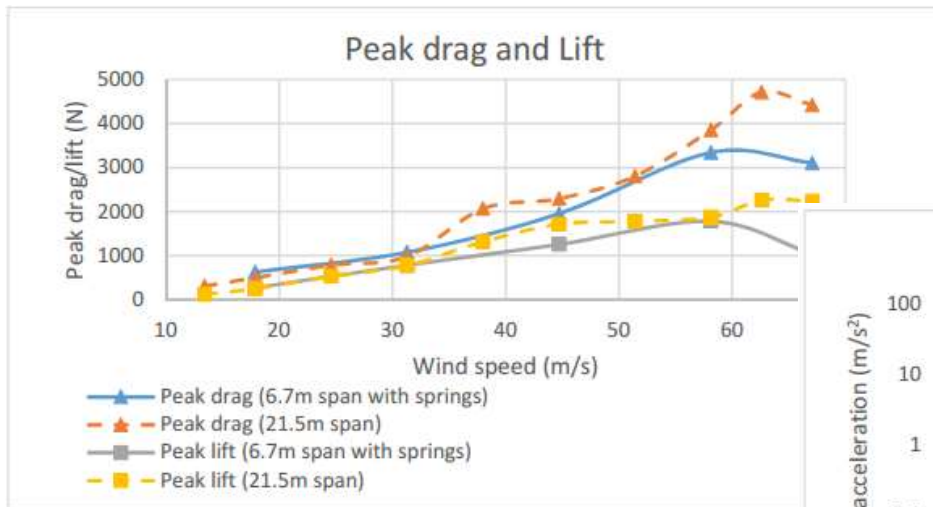
- Test rig with a span of approx. 21 ft
- Objective: span-wire possesses the same deflection versus force relationship as the field span
- Springs added at the ends of the messenger/catenary wires



- Test rig with a span of approx. 75 ft
- Objective: validate short-span test rig



- Vast amount of data was collected



- Removed all instrumentation and increased wind speed up to Cat-5 hurricane (157 mph)

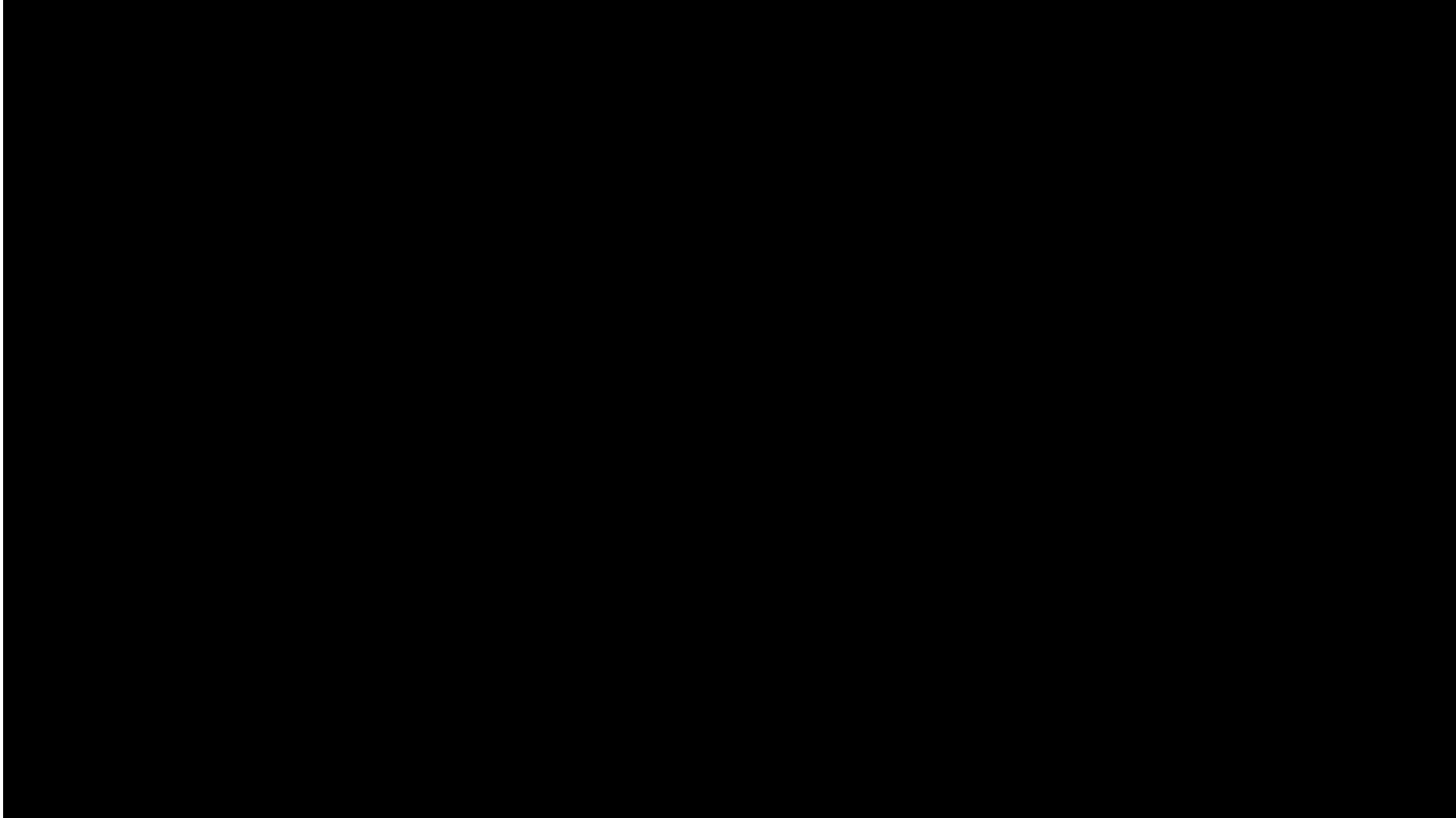


Full-scale Destructive Test – Roof Paver Lift-off Speed



Live Streaming
of Experiments
using
Telepresence at
WOW EF

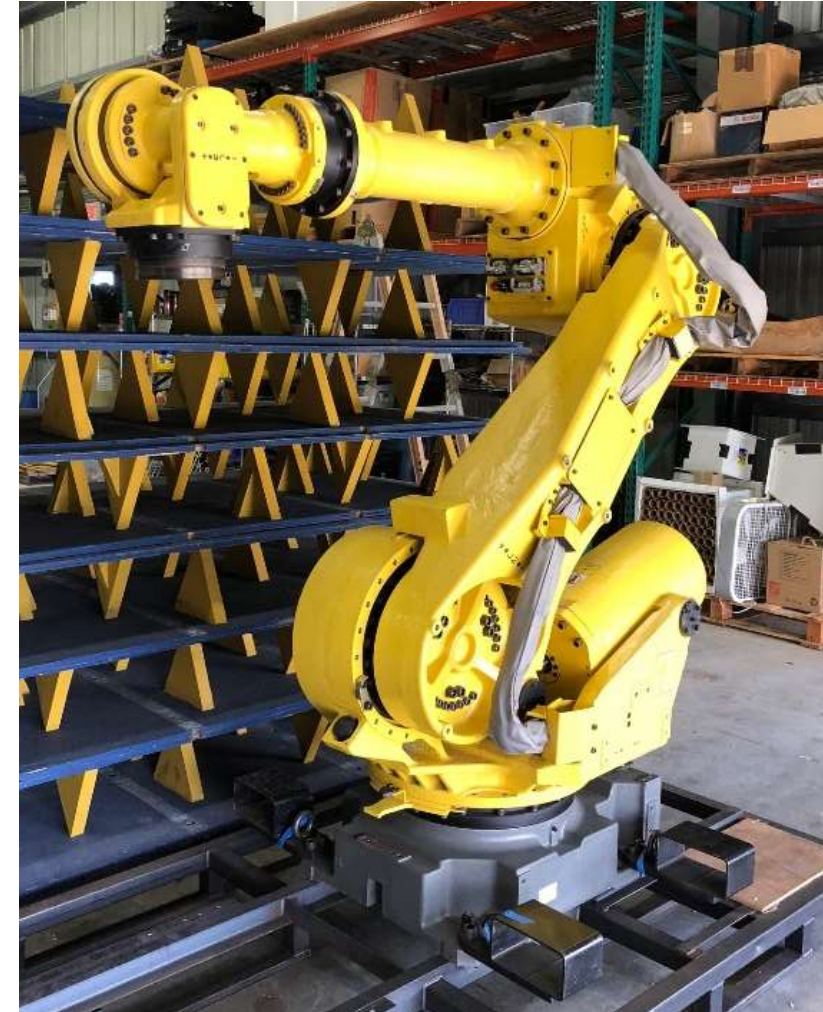
- [Link to IMAX Video](#)



New Capabilities



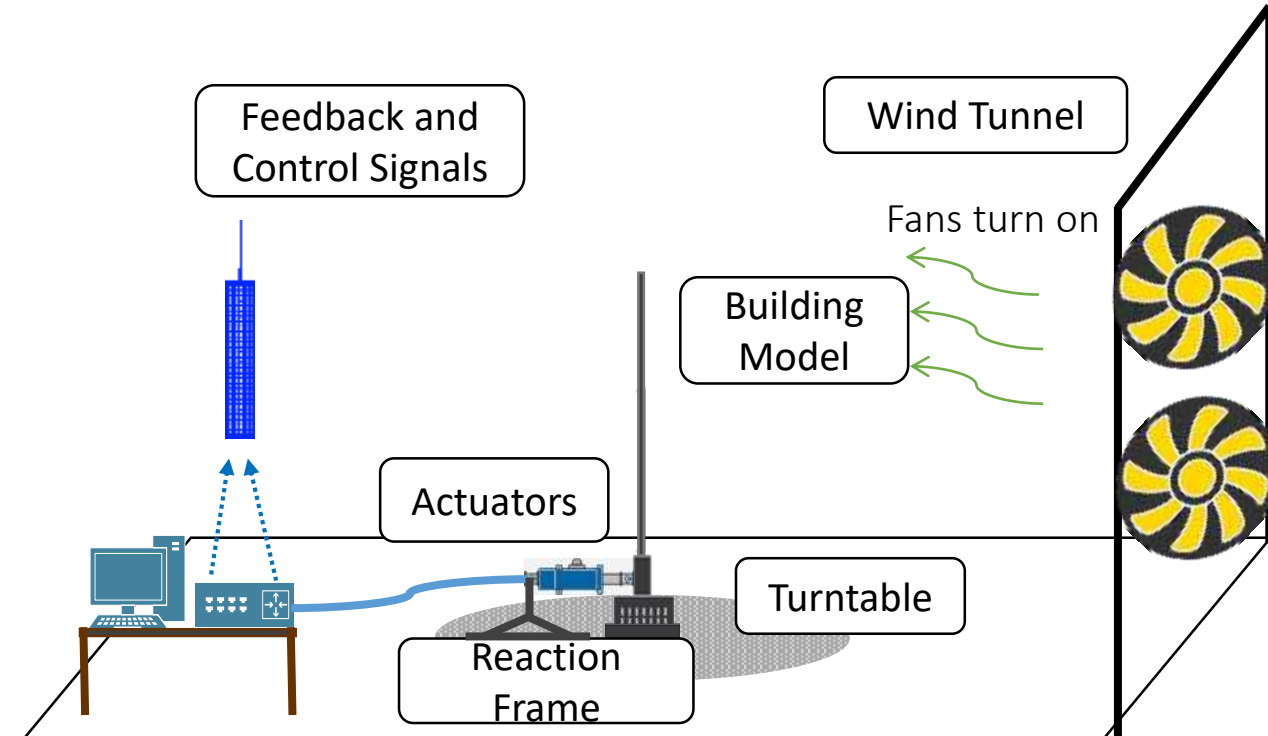
New **Automated Roughness System** will significantly reduce the test time setup.



New **Automated 3-Axis Traverse System** (robot arm) will help to quickly characterize wind field.

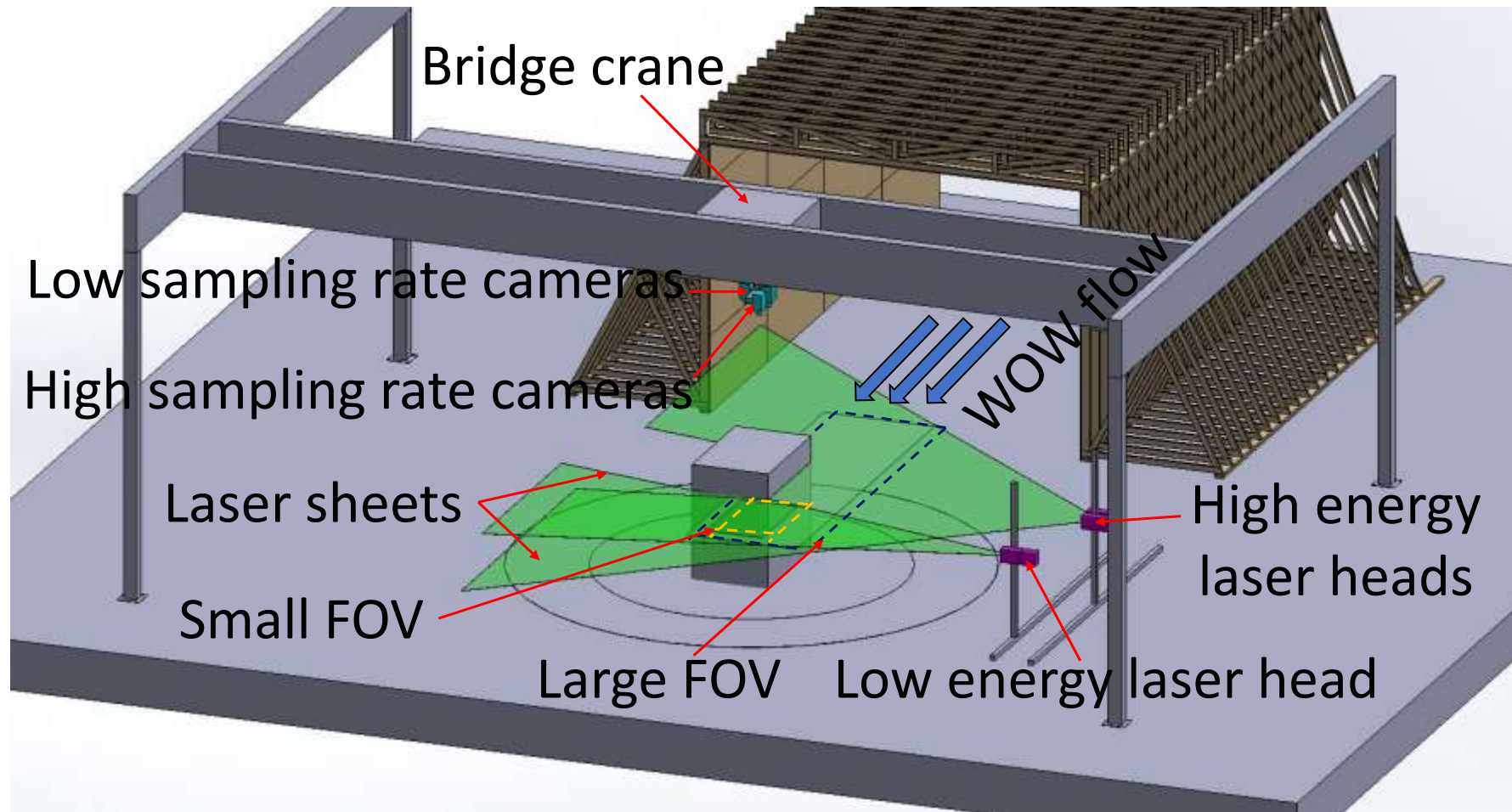


Simulation of **non-synoptic downburst wind flow at large scales** for downburst-structure interaction studies.



Hybrid Simulation capabilities will be implemented.

Acquisition of a **Three Component Particle-Image Velocimetry System** to Enable Fundamental Research in Wind Engineering and Fluid Mechanics (NSF MRI award #1828585)



(a) Horizontal Plane Setup

Q&A Session